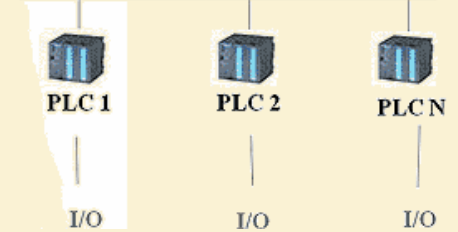
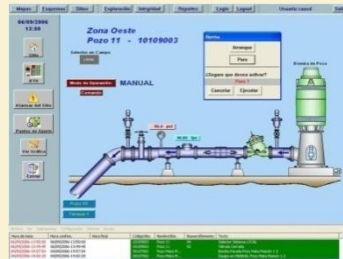
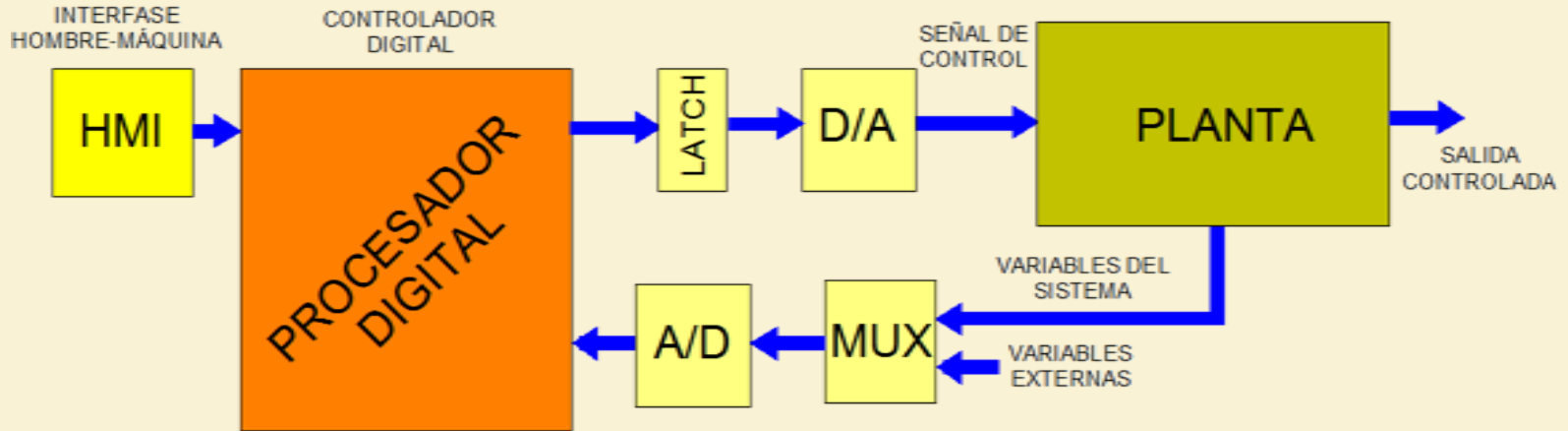


TEORÍA DE CONTROL

SISTEMAS DISCRETOS

SISTEMAS DISCRETOS

ARQUITECTURA DE UN SISTEMA DE CONTROL DIGITAL

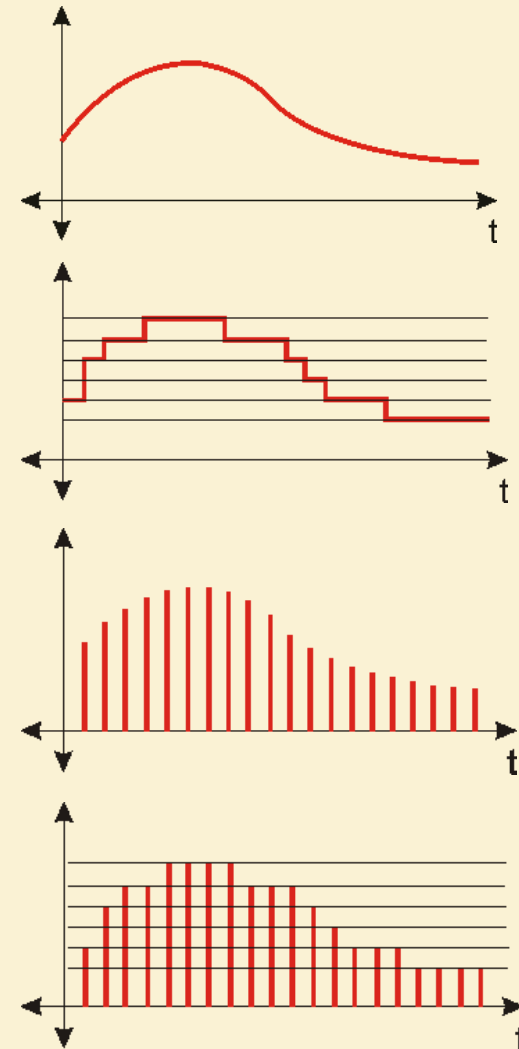


Teoría de Control



SISTEMAS DISCRETOS

TIPOS DE SEÑALES



SISTEMAS DISCRETOS

TRANSFORMADA Z

$$X(z) = \mathcal{Z}\{x(t)\} = \mathcal{Z}\{x(kT)\} = \sum_{k=0}^{\infty} x(kT)z^{-k}$$

$$X(z) = x(0) + x(T)z^{-1} + x(2T)z^{-2} + x(3T)z^{-3} + \dots + x(kT)z^{-k} + \dots$$

ESCALÓN UNITARIO

$$x(t) = \begin{cases} 1 & \text{para } t \geq 0 \\ 0 & \text{para } t < 0 \end{cases} \quad X(z) = 1 + z^{-1} + z^{-2} + z^{-3} + \dots \rightarrow \frac{1}{1-r} = \frac{1}{1-z^{-1}}$$

$$a^k \quad x(k) = \begin{cases} a^k & \text{para } k \geq 0 \\ 0 & \text{para } k < 0 \end{cases} \quad X(z) = 1 + az^{-1} + a^2z^{-2} + a^3z^{-3} + \dots \rightarrow r = az^{-1}$$
$$X(z) = \frac{1}{(1-az^{-1})}$$



SISTEMAS DISCRETOS

TRANSFORMADA Z

$$e^{-at}$$

$$x(t) = \begin{cases} e^{-at} & \text{para } t \geq 0 \\ 0 & \text{para } t < 0 \end{cases}$$

$$X(z) = 1 + e^{-aT} z^{-1} + e^{-2aT} z^{-2} + e^{-3aT} z^{-3} + \dots \rightarrow r = e^{-aT} z^{-1}$$

$$X(z) = \frac{1}{(1 - e^{-aT} z^{-1})}$$

RAMPA UNITARIA

$$x(t) = \begin{cases} t & \text{para } t \geq 0 \\ 0 & \text{para } t < 0 \end{cases}$$

$$X(z) = Tz^{-1} + 2Tz^{-2} + 3Tz^{-3} + \dots =$$

$$= Tz^{-1} (1 + 2z^{-1} + 3z^{-2} + 4z^{-3} + \dots) = \frac{Tz^{-1}}{(1 - z^{-1})^2}$$



TRANSFORMADA Z

PROPIEDADES

$$\mathcal{Z} \{ a x(t) \} = a X(z)$$

$$\mathcal{Z} \{ a x(t) + b y(t) \} = a X(z) + b Y(z)$$

$$\mathcal{Z} \{ a^k x(t) \} = X(a^{-1}z)$$

$$\mathcal{Z} \{ x(t + nT) \} = z^n \left(X(z) - \sum_{k=0}^{n-1} x(kT) z^{-k} \right)$$

$$\mathcal{Z} \{ x(t - nT) \} = z^{-n} X(z)$$

Teorema del Valor inicial

$$f(0) = \lim_{|z| \rightarrow \infty} F(z)$$

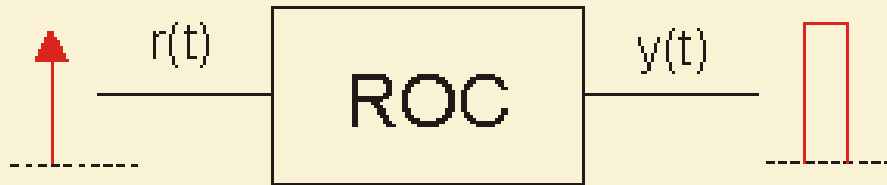
Teorema del Valor Final

$$f(\infty) = \lim_{z \rightarrow 1} (z-1)F(z)$$



SISTEMAS DISCRETOS

RETENCIÓN DE ORDEN CERO

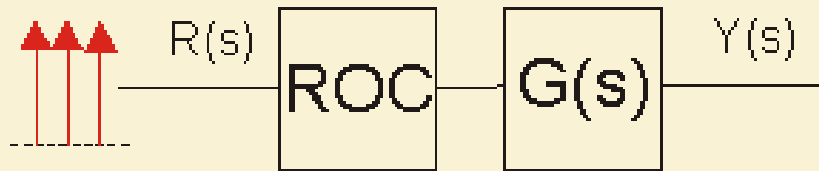


$y(t)$ = respuesta al impulso

$$y(t) = u(t) - u(t - T)$$

$u(t)$ = escalón

$$\frac{Y(s)}{R(s)} = \left[\frac{1}{s} - \frac{1}{s} e^{-sT} \right] = \frac{1 - e^{-sT}}{s} = \text{ROC}$$



$$\frac{Y(s)}{R(s)} = \frac{1 - e^{-sT}}{s} G(s) = (1 - e^{-sT}) G_1(s)$$

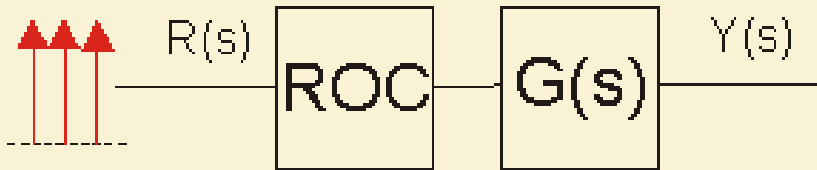
$$X_1(s) = e^{-sT} G_1(s)$$

$$x_1(t) = \int_0^t g_0(t - \tau) g_1(\tau) d\tau \quad g_0(t) = \delta(t - T)$$

$$x_1(t) = \int_0^t \delta(t - T - \tau) g_1(\tau) d\tau = g_1(t - T)$$



RETENCIÓN DE ORDEN CERO



$$\mathcal{Z} \{g_1(t)\} = G_1(z)$$

$$\frac{Y(s)}{R(s)} = \frac{1 - e^{-sT}}{s} G(s)$$

$$\mathcal{Z} \{x_1(t)\} = \mathcal{Z} \{g_1(t - T)\} = z^{-1} G_1(z)$$

$$\frac{Y(z)}{R(z)} = \mathcal{Z} \{G_1(s) - e^{-sT} G_1(s)\}$$

$$\frac{Y(z)}{R(z)} = G_1(z) - z^{-1} G_1(z)$$

$$\frac{Y(z)}{R(z)} = (1 - z^{-1}) G_1(z)$$

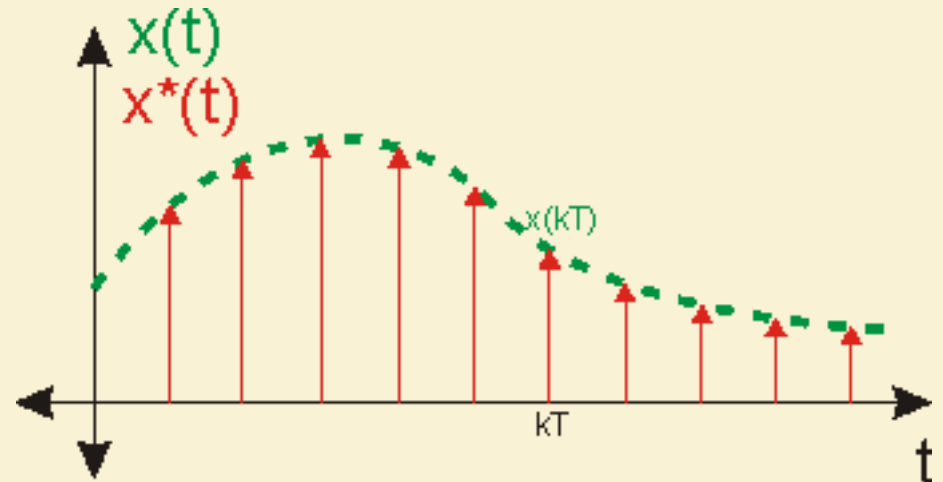
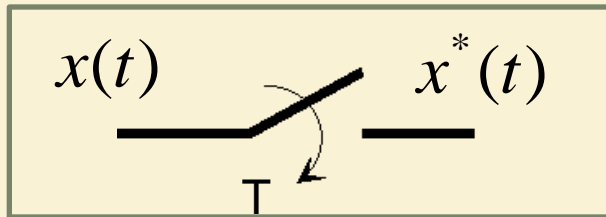
$$\frac{Y(z)}{R(z)} = (1 - z^{-1}) \mathcal{Z} \left\{ \frac{G(s)}{s} \right\}$$



MUESTREO MEDIANTE IMPULSOS

$$x^*(t) = \sum_{k=0}^{\infty} x(kT)\delta(t - kT)$$

$$\delta_T(t - kT) = \sum_{k=0}^{\infty} \delta(t - kT)$$



$$X^*(s) = x(0)\mathcal{L}\{\delta(t)\} + x(T)\mathcal{L}\{\delta(t-T)\} + \dots$$

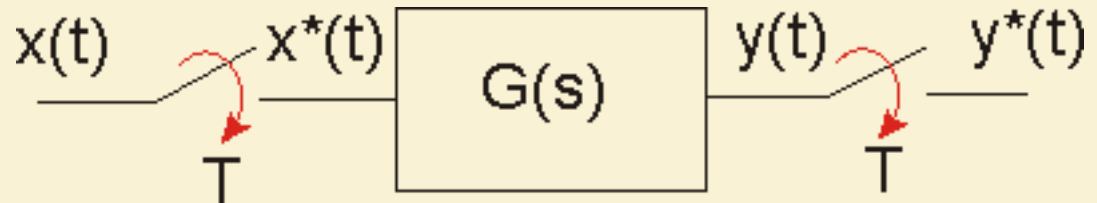
$$X^*(s) = x(0) + x(T)e^{-sT} + x(2T)e^{-2sT} + \dots$$

$$X^*(s) = \sum_{k=0}^{\infty} x(kT)e^{-skT} = X(z) \quad \text{con } z = e^{sT}$$



SISTEMAS DISCRETOS

FUNCIÓN TRANSFERENCIA DE PULSO



$$\mathcal{Z} \{ y(t) \} = Y(z) = \sum_{k=0}^{\infty} y(kT) z^{-k}$$

$$y(t) = \int_0^t g(t-\tau) x^*(\tau) d\tau = \int_0^t x^*(t-\tau) g(\tau) d\tau$$

$$x^*(t) = \sum_{k=0}^{\infty} x(kT) \delta(t-kT)$$

La respuesta de $y(t)$ es la suma de las respuestas al impulso

$$y(t) = \begin{cases} g(t)x(0) & 0 \leq t < T \\ g(t)x(0) + g(t-T)x(T) & T \leq t < 2T \\ \dots & \dots \\ g(t)x(0) + g(t-T)x(T) + \dots + g(t-kT)x(kT) + \dots & kT \leq t < (k+1)T \end{cases}$$



FUNCIÓN TRANSFERENCIA DE PULSO

$$y(t) = \sum_{h=0}^{\infty} g(t-hT) x(hT)$$

$$y(kT) = \sum_{h=0}^{\infty} g(kT-hT) x(hT) \quad \text{Sumatoria de Convolución}$$

$$y(kT) = x(kT) * g(kT)$$

$$Y(z) = \sum_{k=0}^{\infty} y(kT) z^{-k}$$

$$Y(z) = \sum_{k=0}^{\infty} \sum_{h=0}^{\infty} g(kT-hT) x(hT) z^{-k} \quad m = k - h$$

$$Y(z) = \sum_{m=0}^{\infty} \sum_{h=0}^{\infty} g(mT) x(hT) z^{-m-h}$$

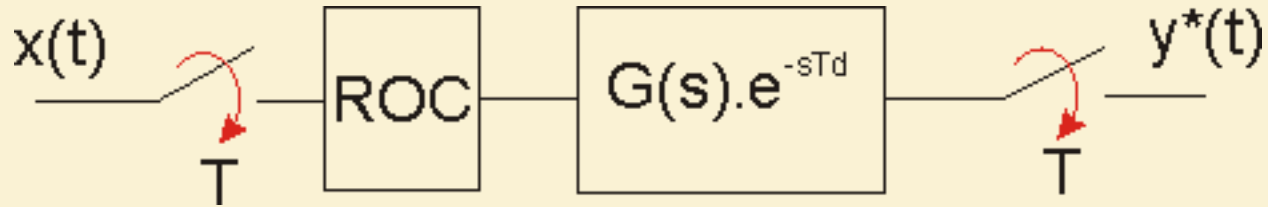
$$Y(z) = \sum_{m=0}^{\infty} g(mT) z^{-m} \cdot \sum_{h=0}^{\infty} x(hT) z^{-h}$$

$$Y(z) = G(z) \cdot X(z)$$



SISTEMAS DISCRETOS

SISTEMAS CON RETARDO



$$\frac{Y(z)}{X(z)} = (1 - z^{-1}) \mathcal{Z} \left\{ \frac{G(s)}{s} e^{-sT_d} \right\}$$

$$\frac{Y(z)}{X(z)} = (1 - z^{-1}) z^{-\frac{T_d}{T}} \mathcal{Z} \left\{ \frac{G(s)}{s} \right\}$$

Si $T_d = N.T$

$$\frac{Y(z)}{X(z)} = (1 - z^{-1}) z^{-N} \mathcal{Z} \left\{ \frac{G(s)}{s} \right\}$$



SISTEMAS DISCRETOS

TABLA DE TRANSFORMADA Z

Si bien la transformada Z se define en el dominio temporal existen tablas que permiten transformar al plano Z expresiones representadas en el campo transformado de Laplace.

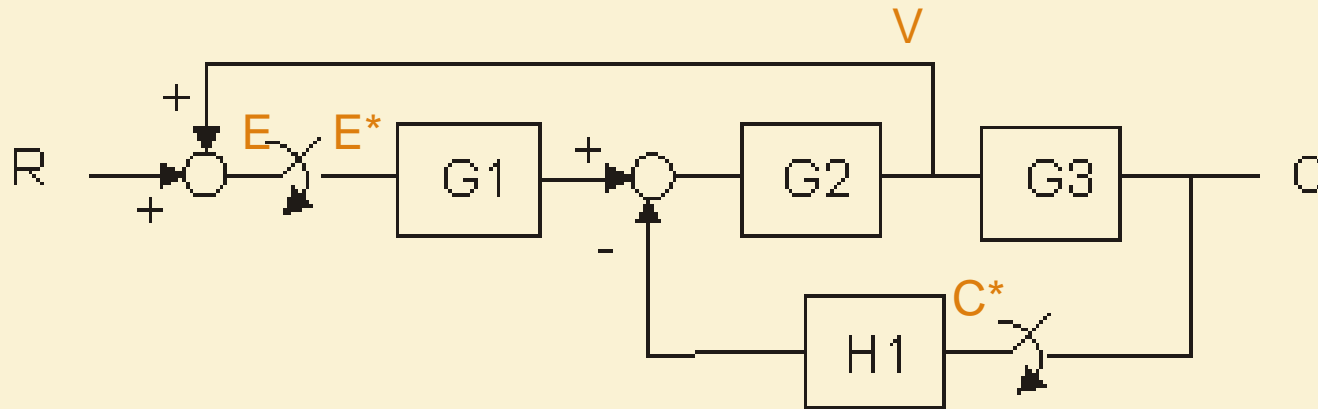
$f(t)$ F. Continua	$f(kT)$ F. Discreta, muestreada	$F(s)$ Transformada de Laplace	$F(Z)$ Transformada Z
$\delta(t)$ Impulso de Dirac	$\delta(kT)$	1	1
$\delta(t - T)$	$\delta(t - kT)^*$	e^{-sT}	
$v(t)$ Escalón Unitario	$v(kT)$	$\frac{1}{s}$	$\frac{Z}{Z-1}$
$v(t - T)$	$v(t - kT)^*$	$\frac{e^{-sT}}{s}$	
	$v(t - kT - T\omega)$	$\frac{e^{-s(kT + T\omega)}}{s}$	
t Rampa	kT	$\frac{1}{s^2}$	$\frac{Tz}{(z-1)^2}$
t^2	$(kT)^2$	$\frac{2}{s^3}$	$\frac{T^2 z(z+1)}{(z-1)^3}$
t^3	$(kT)^3$	$\frac{6}{s^4}$	$\frac{T^3 z(z^2 + 4z + 1)}{(z-1)^4}$
$\frac{1}{2}t^2$	$\frac{1}{2}(kT)^2$	$\frac{1}{s^3}$	$\frac{T^2 z(z+1)}{2(z-1)^3}$
$t^{m-1};$ $m = 1, 2, 3, \dots$		$\frac{(m-1)!}{s^m}$	$\lim_{b \rightarrow 0} (-1)^{m-1} \left(\frac{\partial^{m-1}}{\partial b^{m-1}} \left[\frac{z}{z - e^{-bT}} \right] \right)$
e^{-at}	e^{-akT}	$\frac{1}{s+a}$	$\frac{Z}{Z - e^{-aT}}$
te^{-at}	$kT e^{-akT}$	$\frac{1}{(s+a)^2}$	$\frac{T e^{-aT} z}{(z - e^{-aT})^2}$
$t^2 e^{-at}$	$(kT)^2 e^{-akT}$	$\frac{2}{(s+a)^3}$	$\frac{T^2 e^{-aT} z(z + e^{-aT})}{(z - e^{-aT})^3}$
$\sin(bt)$	$\sin(bkT)$	$\frac{b}{s^2 + b^2}$	$\frac{z \sin(bT)}{z^2 - 2z \cos(bT) + 1}$
$\cos(bt)$	$\cos(bkT)$	$\frac{s}{s^2 + b^2}$	$\frac{z^2 - z \sin(bT)}{z^2 - 2z \cos(bT) + 1}$
$e^{-at} \sin(bt)$	$e^{-akT} \sin(bkT)$	$\frac{b}{(s+a)^2 + b^2}$	$\frac{z e^{-aT} \sin(bT)}{z^2 - 2z e^{-aT} \cos(bT) + e^{-2aT}}$
$e^{-at} \cos(bt)$	$e^{-akT} \cos(bkT)$	$\frac{s+a}{(s+a)^2 + b^2}$	$\frac{z^2 - z e^{-aT} \cos(bT)}{z^2 - 2z e^{-aT} \cos(bT) + e^{-2aT}}$



SISTEMAS DISCRETOS

EJEMPLO:

El siguientes diagrama representa un sistema muestreado de control. Obtenga una expresión para la salida $C(z)$ cuando se le aplica una entrada $R(s)$ en forma de escalón de amplitud unitaria.



$$E = R + V = R + (E^* G1 - C^* H1)G2 = R + E^* G1G2 - C^* H1G2$$

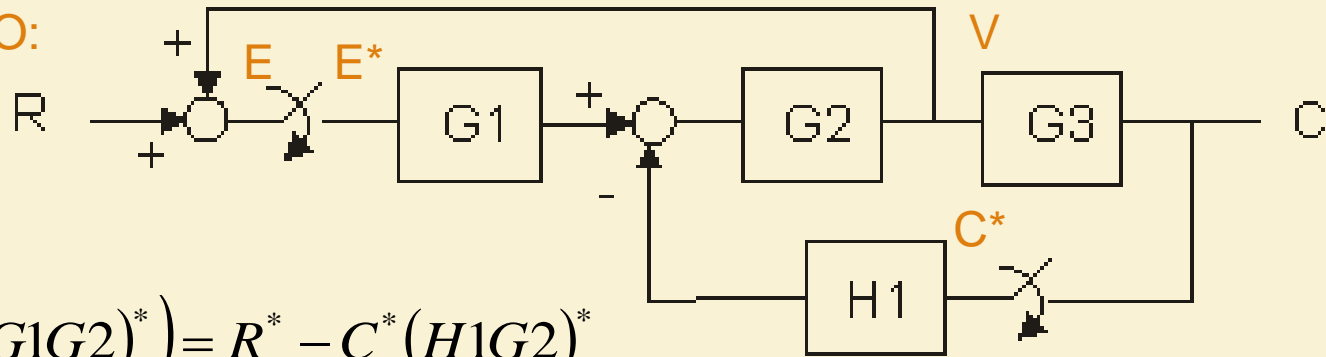
$$E^* = R^* + E^* (G1G2)^* - C^* (H1G2)^*$$

$$E^* (1 - (G1G2)^*) = R^* - C^* (H1G2)^*$$



SISTEMAS DISCRETOS

EJEMPLO:



$$E^* (1 - (G1G2)^*) = R^* - C^* (H1G2)^*$$

$$E^* = \frac{R^* - C^* (H1G2)^*}{(1 - (G1G2)^*)}$$

$$C = (E^* G1 - C^* H1) G2 G3 = E^* G1 G2 G3 - C^* H1 G2 G3$$

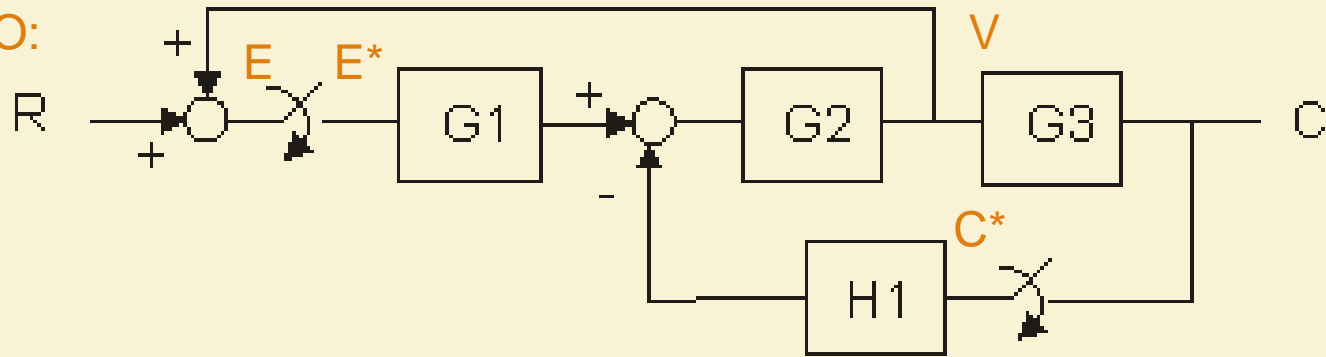
$$C^* = E^* (G1 G2 G3)^* - C^* (H1 G2 G3)^*$$

$$C^* = \frac{R^* - C^* (H1 G2)^*}{(1 - (G1 G2)^*)} (G1 G2 G3)^* - C^* (H1 G2 G3)^*$$



SISTEMAS DISCRETOS

EJEMPLO:



$$C^* = \frac{R^* (G1G2G3)^* - C^* (H1G2)^* (G1G2G3)^* - C^* (H1G2G3)^* (1 - (G1G2)^*)}{(1 - (G1G2)^*)}$$

$$C^* (1 - (G1G2)^*) = R^* (G1G2G3)^* - C^* (H1G2)^* (G1G2G3)^* - C^* (H1G2G3)^* (1 - (G1G2)^*)$$

$$C^* (1 - (G1G2)^* + (H1G2)^* (G1G2G3)^* + (H1G2G3)^* (1 - (G1G2)^*)) = R^* (G1G2G3)^*$$

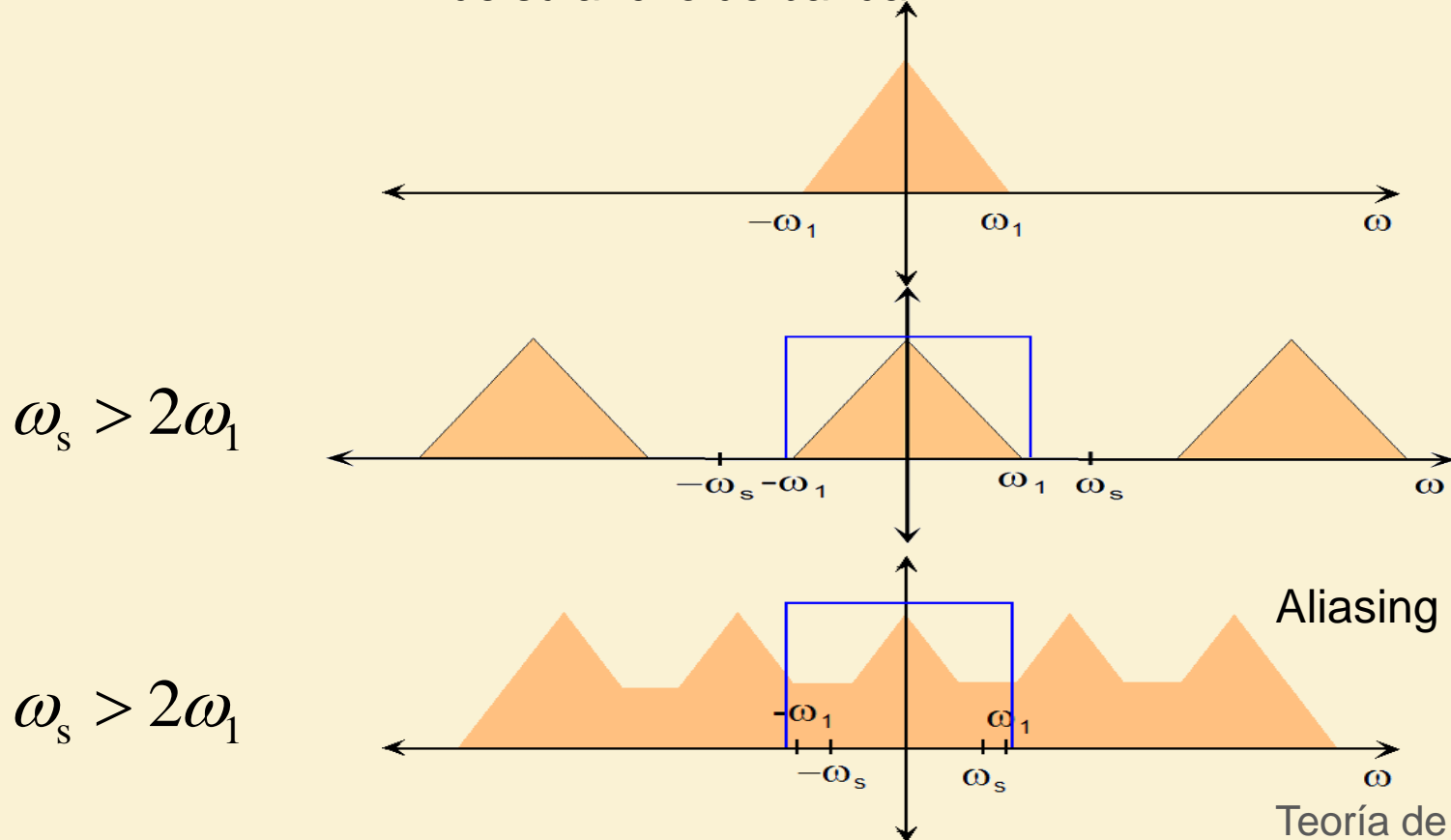
$$C^* = \frac{R^* (G1G2G3)^*}{(1 - (G1G2)^* + (H1G2)^* (G1G2G3)^* + (H1G2G3)^* (1 - (G1G2)^*))}$$

$$C(z) = \frac{R(z)(G1G2G3)(z)}{(1 - (G1G2)(z) + (H1G2)(z)(G1G2G3)(z) + (H1G2G3)(z)(1 - (G1G2)(z)))}$$

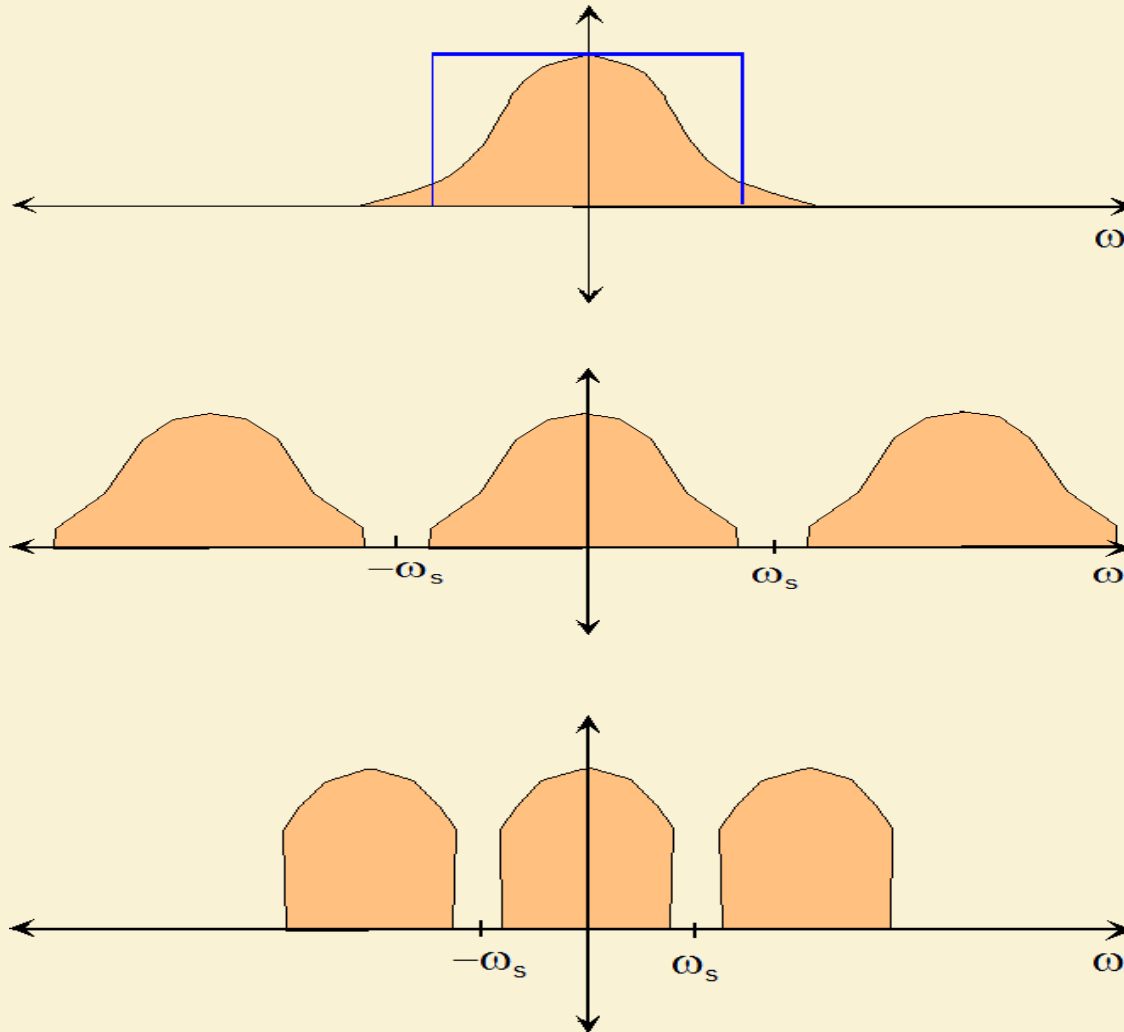


Teorema del muestreo

El teorema demuestra que la reconstrucción exacta de una señal periódica continua en banda base a partir de sus muestras, es matemáticamente posible si la señal está limitada en banda y la tasa de muestreo es superior al doble de su ancho de banda.

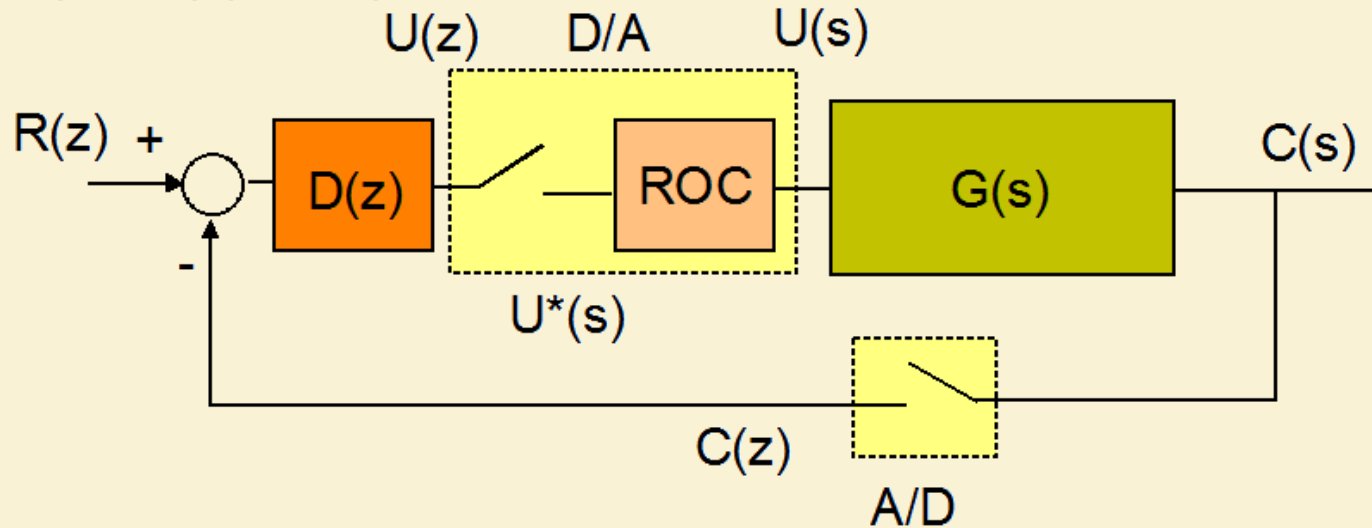


FILTRO ANTI ALIASING



SISTEMAS DISCRETOS

CONTROL DISCRETO



$$\frac{C(s)}{U^*(s)} = \frac{1 - e^{-sT}}{s} G(s)$$

$$G(z) = \frac{C(z)}{U(z)} = (1 - z^{-1}) \mathbf{Z} \left\{ \frac{G(s)}{s} \right\}$$

$$\frac{C(z)}{R(z)} = \frac{G(z)D(z)}{1 + G(z)D(z)}$$



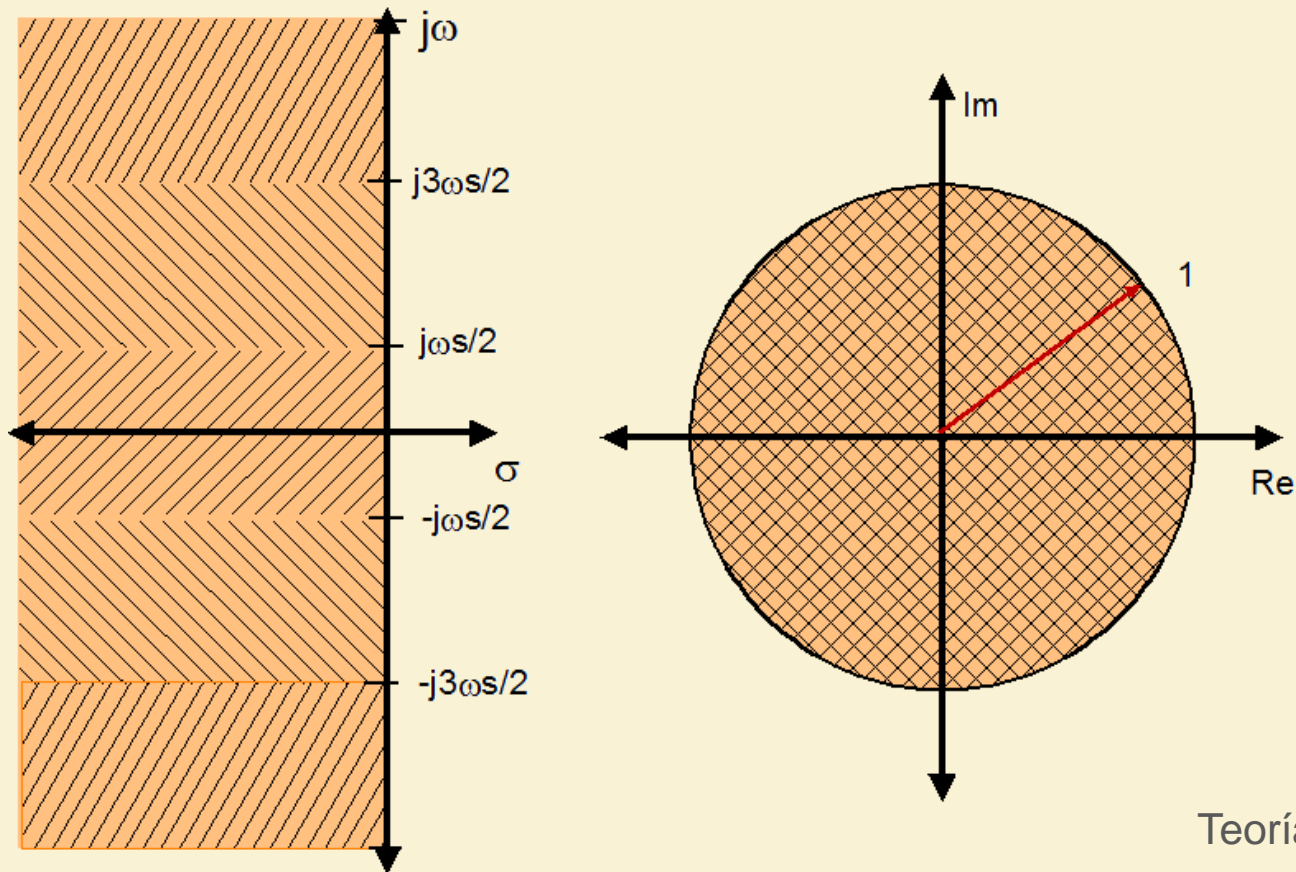
SISTEMAS DISCRETOS

CORRESPONDENCIA ENTRE EL PLANO S Y EL PLANO Z

$$z = e^{sT} \quad \text{con} \quad s = \sigma + j\omega$$

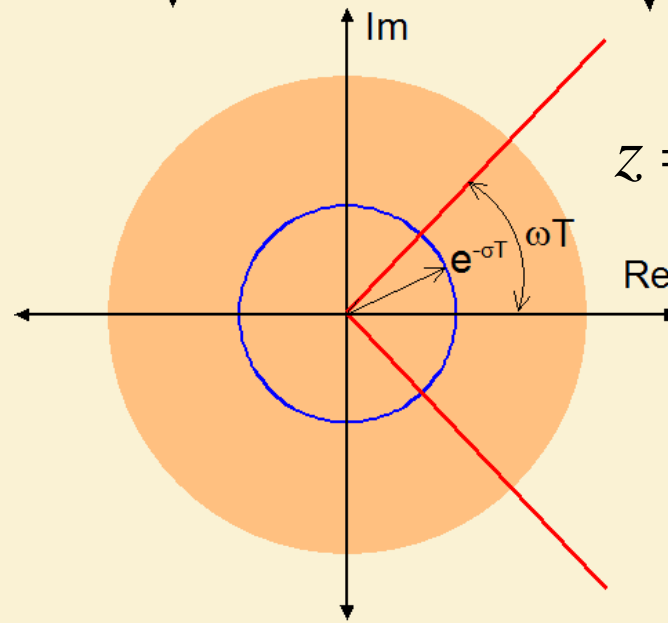
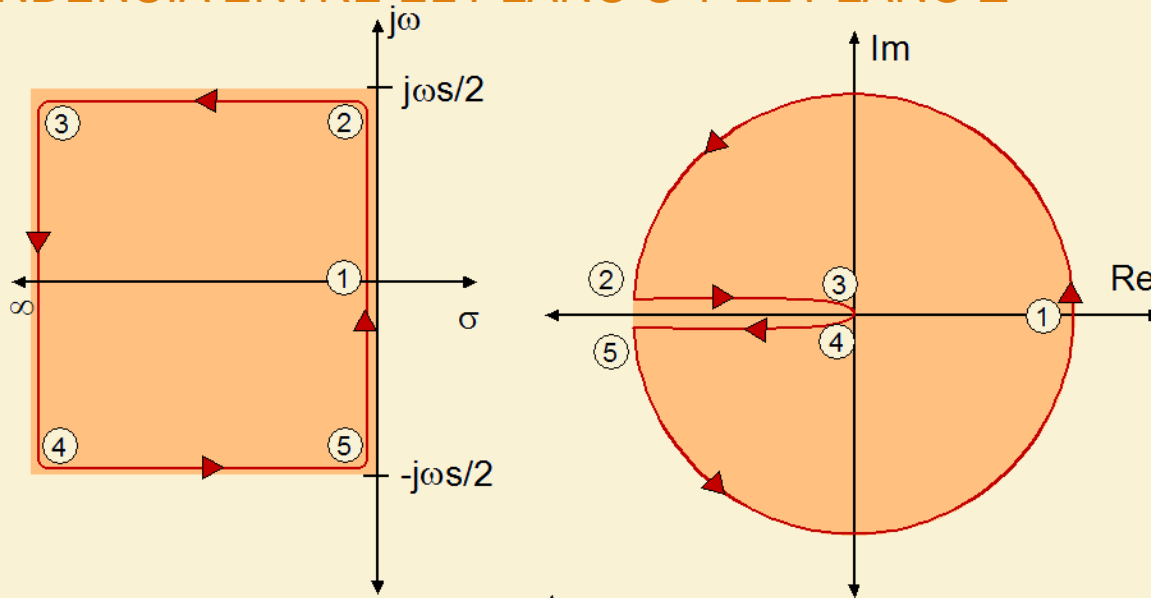
$$z = e^{(\sigma + j\omega)T} = e^{\sigma T} e^{j\omega T} = e^{\sigma T} e^{j(\omega T + 2\pi k)}$$

$$|z| = e^{\sigma T} < 1$$



SISTEMAS DISCRETOS

CORRESPONDENCIA ENTRE EL PLANO S Y EL PLANO Z

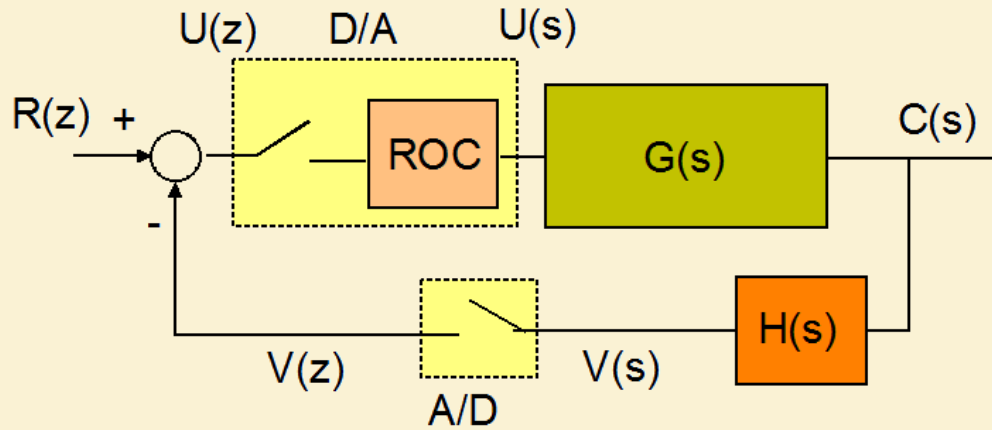


$$z = e^{(-\sigma + j\omega)T} = e^{-\sigma T} e^{j\omega T}$$



SISTEMAS DISCRETOS

ANÁLISIS DE ESTABILIDAD



$$GH(z) = \frac{V(z)}{U(z)} = (1 - z^{-1}) \mathcal{Z} \left\{ \frac{GH(s)}{s} \right\}$$

$$\frac{C(z)}{R(z)} = \frac{G(z)}{1 + GH(z)}$$

$$P(z) = 1 + GH(z) = 0$$

$$G(s) = \frac{1}{s(s+1)} \quad H(s) = 1 \quad T = 1$$

$$G(z) = (1 - z^{-1}) \mathcal{Z} \left\{ \frac{1}{s^2} - \frac{1}{s} + \frac{1}{(s+1)} \right\}$$

$$G(z) = \frac{(z-1)}{z} \left[\frac{Tz}{(z-1)^2} - \frac{z}{(z-1)} + \frac{z}{(z-e^{-T})} \right]$$



ANÁLISIS DE ESTABILIDAD

$$G(z) = \frac{(z-1)}{z} \left[\frac{z(T(z-e^{-T}) - (z-1)(z-e^{-T}) + (z-1)^2)}{(z-1)^2(z-e^{-T})} \right]$$

$$G(z) = \left[\frac{z(T + e^{-T} - 1) + (1 - e^{-T} - Te^{-T})}{(z-1)(z-e^{-T})} \right]$$

$$G(z) = \frac{0,3679(z + 0,7183)}{(z-1)(z-0,3679)}$$

$$P(z) = (z-1)(z-0,3679) + 0,3679z + 0,2642 = z^2 - z + 0,6321$$

$$z_1 = 0,5 + j0,6182 \quad z_2 = 0,5 - j0,6182$$

$$|z_1| = |z_2| = 0,7950919 < 1 \quad \text{ESTABLE}$$

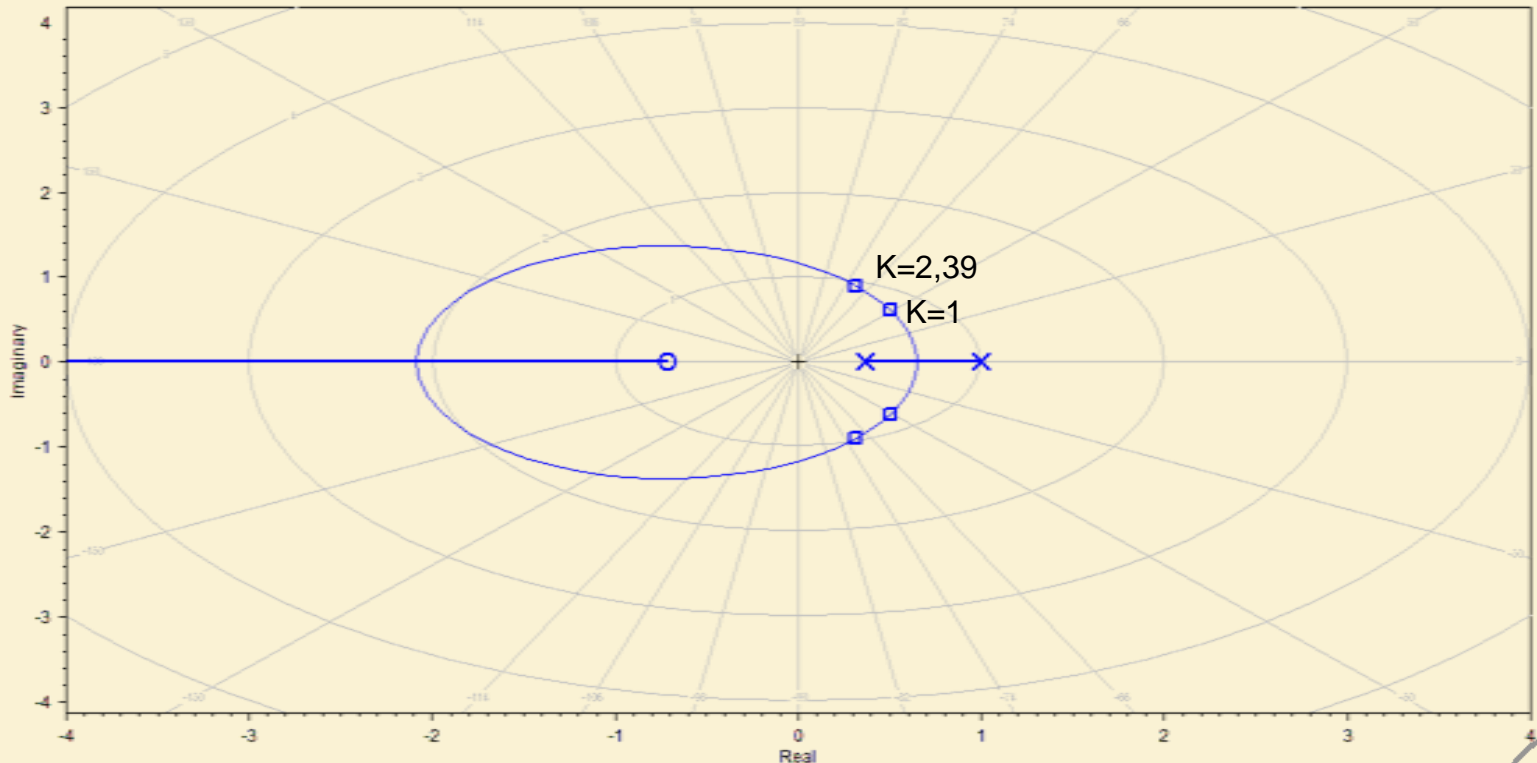


SISTEMAS DISCRETOS

ANÁLISIS DE ESTABILIDAD

$$G(s) = \frac{K}{s(s+1)} \quad H(s)=1 \quad T=1$$

$$G(z) = \frac{0,3679K(z+0,7183)}{(z-1)(z-0,3679)}$$



ANÁLISIS DE ESTABILIDAD

Si el periodo de muestreo T no es conocido

$$G(z) = \left[\frac{z(T + e^{-T} - 1) + (1 - e^{-T} - Te^{-T})}{(z-1)(z - e^{-T})} \right]$$

$$1 + G(z) = \frac{(z-1)(z - e^{-T}) + [z(T + e^{-T} - 1) + (1 - e^{-T} - Te^{-T})]}{(z-1)(z - e^{-T})}$$

$$1 + G(z) = \frac{z^2 + (T - 2)z - Te^{-T} + 1}{(z-1)(z - e^{-T})}$$

Para $T=3.923$

$$1 + G(z) = \frac{z^2 + 1,923z + 0,9224}{(z-1)(z - 0,01978)}$$

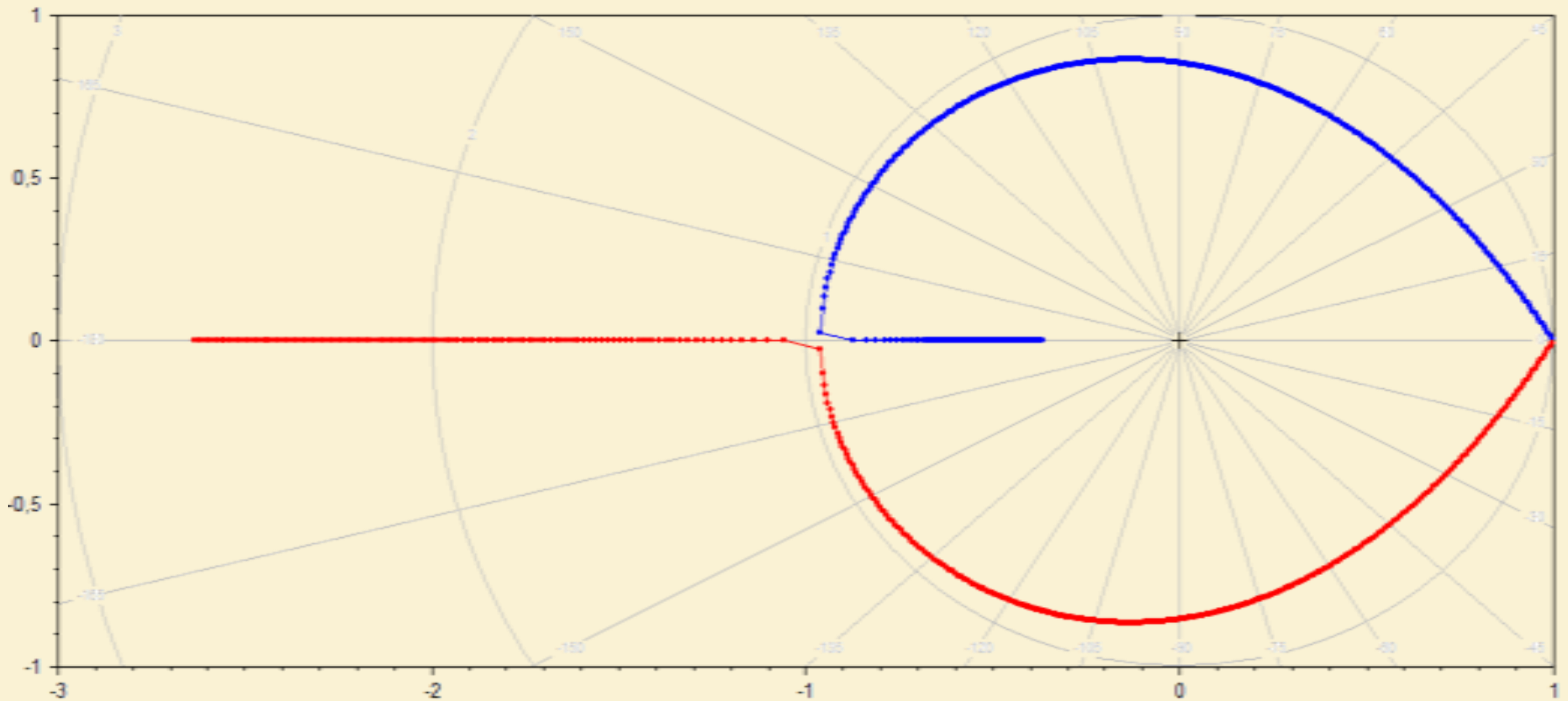
Y los ceros son $z_1 = -0,91583$ y $z_2 = -1,00716$



SISTEMAS DISCRETOS

ANÁLISIS DE ESTABILIDAD

$$1 + G(z) = \frac{z^2 + (T - 2)z - Te^{-T} + 1}{(z - 1)(z - e^{-T})}$$



SISTEMAS DISCRETOS

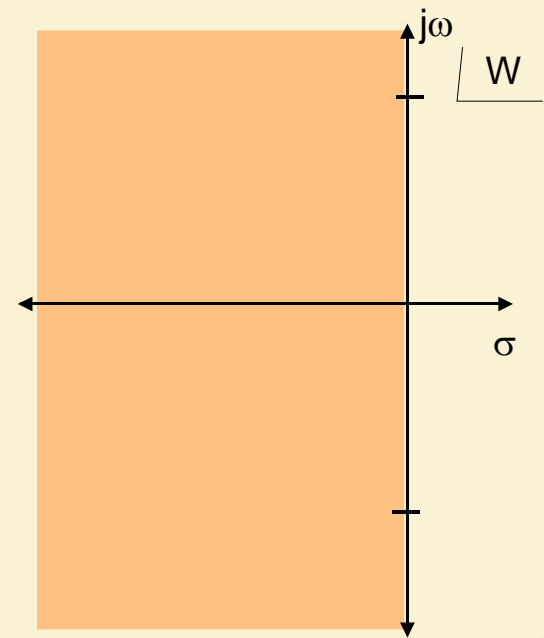
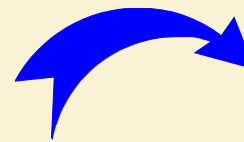
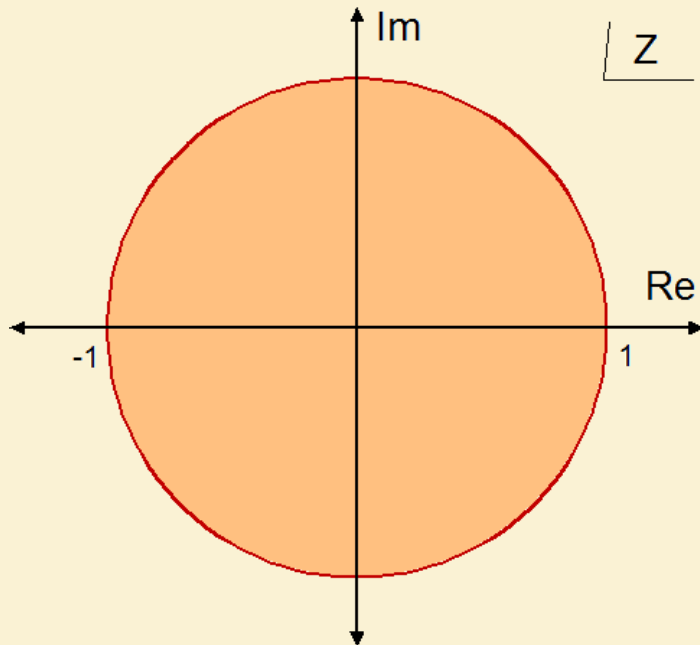
TRANSFORMACIÓN BILINEAL

$$z = 1_{\angle\phi} = e^{j\phi}$$

$$w = \frac{2}{T} \frac{(e^{j\phi} - 1)}{(e^{j\phi} + 1)} = \frac{2}{T} \frac{\left(\frac{e^{j\frac{\phi}{2}} - e^{-j\frac{\phi}{2}}}{e^{j\frac{\phi}{2}} + e^{-j\frac{\phi}{2}}} \right)}{j \frac{2 \operatorname{sen}\left(\frac{\phi}{2}\right)}{\cos\left(\frac{\phi}{2}\right)}}$$

$$w = \frac{2}{T} \frac{(z-1)}{(z+1)}$$

$$z = \frac{\left(1 + \frac{wT}{2}\right)}{\left(1 - \frac{wT}{2}\right)}$$



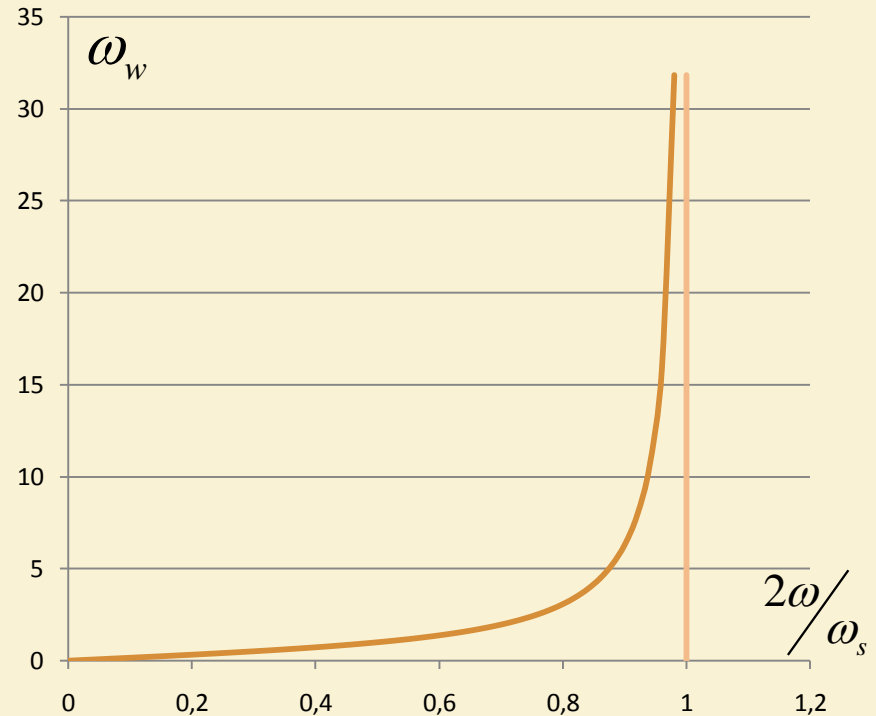
SISTEMAS DISCRETOS

TRANSFORMACIÓN BILINEAL

$$z = e^{sT} \Big|_{s=j\omega} = e^{j\omega T}$$

$$w = \frac{2(z-1)}{T(z+1)}$$

$$w = j \frac{2}{T} \frac{\operatorname{sen}\left(\frac{\omega T}{2}\right)}{\cos\left(\frac{\omega T}{2}\right)} = j \frac{2}{T} \tan\left(\frac{\omega T}{2}\right)$$



$$\text{si } \left(\frac{\omega T}{2}\right) \ll 1 \quad w = \sigma_w + j\omega_w \approx j \frac{2}{T} \left(\frac{\omega T}{2}\right) \quad \omega_w \approx \omega$$



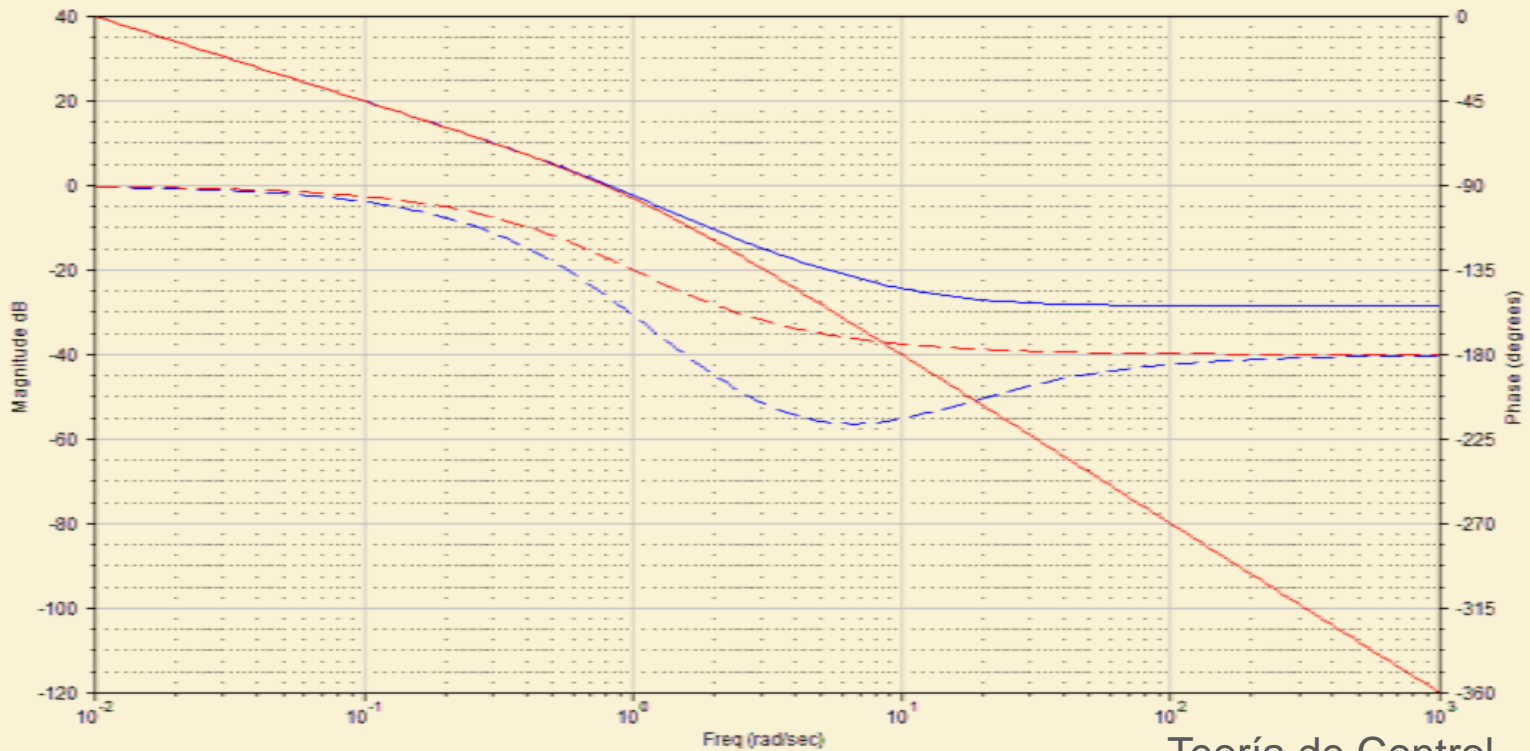
SISTEMAS DISCRETOS

TRANSFORMACIÓN BILINEAL

$$G(s) = \frac{1}{s(s+1)} \quad H(s)=1 \quad T=1$$

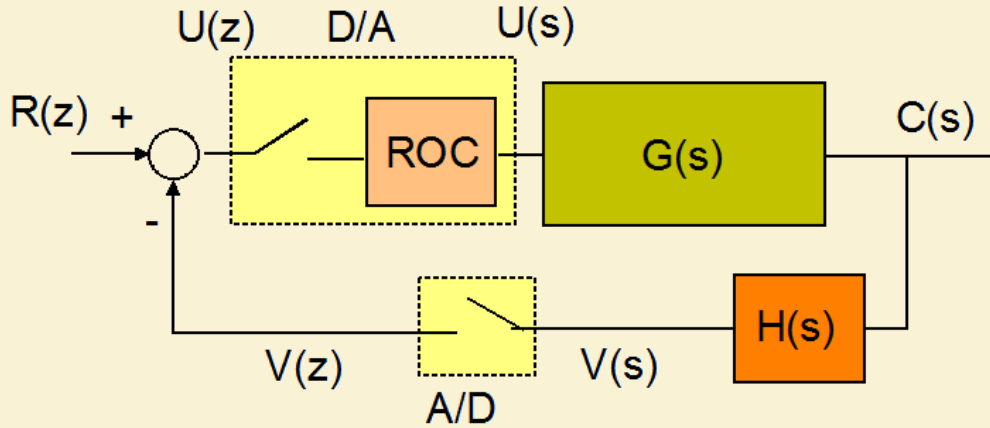
$$G(z) = \frac{0,3679(z+0,7183)}{(z-1)(z-0,3679)}$$

$$G(w) = \frac{-0,03788(w+12,2)(w-2)}{w(w+0,9242)}$$



SISTEMAS DISCRETOS

APROXIMACIÓN DE LA RETENCIÓN DE ORDEN CERO



$$G_{ROC}(j\omega) = T \frac{\text{sen}\left(\frac{\omega\pi}{\omega_s}\right)}{\left(\frac{\omega\pi}{\omega_s}\right)} e^{-j\left(\frac{\omega\pi}{\omega_s}\right)}$$

$$G_{ROC}(j\omega)GH^*(j\omega) = \frac{1}{T} \sum_{-\infty}^{\infty} G_{ROC}(j\omega + jn\omega_s)GH(j\omega + jn\omega_s)$$

$$G_{ROC}(j\omega)GH^*(j\omega) = \frac{1}{T} \sum_{-\infty}^{\infty} T \frac{\text{sen}\left(\frac{\omega + n\omega_s}{2}\right)}{\left(\frac{\omega + n\omega_s}{2}\right)} e^{-j\left(\frac{\omega + n\omega_s}{2}\right)T} GH(j\omega + jn\omega_s)$$

$$G_{ROC}(j\omega)GH^*(j\omega) = GH(j\omega)e^{-j\omega T/2}$$



SISTEMAS DISCRETOS

APROXIMACIÓN DE LA RETENCIÓN DE ORDEN CERO

